

二軸スクリュ押出機の一般化Hele-Shaw流れ定式化に基づくFEM解析

FEM simulation based on
generalized Hele-Shaw flow formulation
for twin screw extruder

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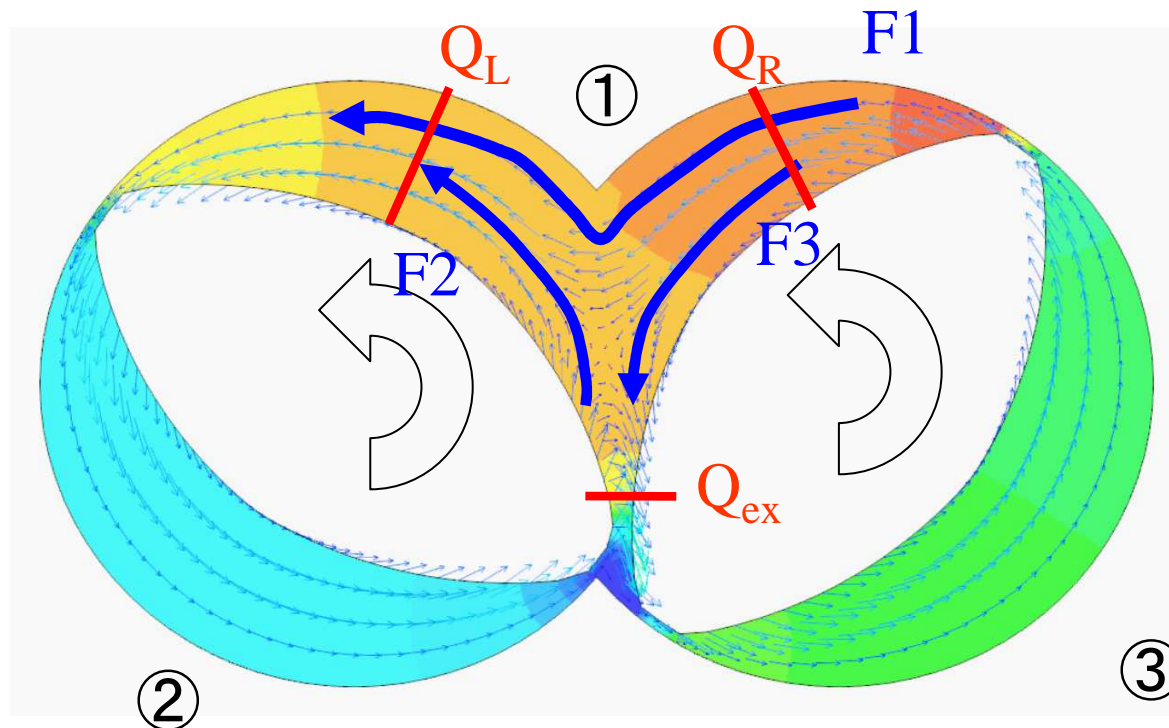
□ Background

Comparison of analysis method for twin screw extruder

Method	Accuracy	Computational cost	Availability	Operability
3D	◎	△	○	△
1D	△	◎	△	◎
2.5D	○	○	○	○

◎ : Excellent, ○ : Good, △ : Moderate

□ Modeling method



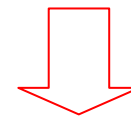
Self wipe intermeshing co-rotating twin screw

F1:right to left flow

F2:left to left flow

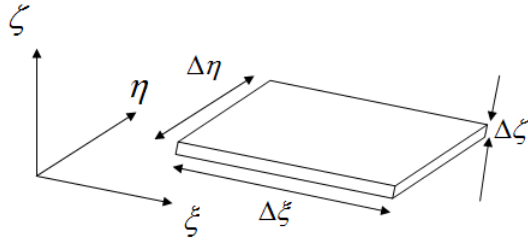
F3:right to right flow

$Q_{ex} \doteq 0$ on the average estimation
in the thickness direction



$$Q_L = Q_R$$

Generalized Hele-Shaw Formulation



Assumption:

$$\frac{\partial p}{\partial \zeta} = 0 \quad \text{Good}$$

$$\left| \frac{\partial U}{\partial \zeta} \right| \gg \left| \frac{\partial U}{\partial \xi} \right|, \left| \frac{\partial U}{\partial \eta} \right| \quad \text{Doubtful, but...}$$

Variable: (u,v,w,p)

$$\eta \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) = \frac{\partial p}{\partial x},$$

$$\eta \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right) = \frac{\partial p}{\partial y},$$

$$\eta \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right) = \frac{\partial p}{\partial z},$$

$$\left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) = 0$$

Variable: (S, p)

$$\langle u \rangle = -S \frac{\partial p}{\partial x} + \Phi_x,$$

$$\langle v \rangle = -S \frac{\partial p}{\partial y} + \Phi_y,$$

$$\langle w \rangle = -S \frac{\partial p}{\partial z},$$

$$\left(\frac{\partial}{\partial x} \left(-S \frac{\partial p}{\partial x} + \Phi_x \right) + \frac{\partial}{\partial y} \left(-S \frac{\partial p}{\partial y} + \Phi_y \right) + \frac{\partial}{\partial z} \left(-S \frac{\partial p}{\partial z} \right) \right) = 0$$

An efficient method for generating of the FEA model

Twin Screw Modeling Thermal Boundary Condition set Analysis

Intermeshing Type
Intermeshing Co-rotating Block Number 4

Barrel radius(mm) 20 Distance between Axis(mm) 32.85 Clearance(mm) 0.5 Total Screw Length(mm) 350 L/D 8.75

Screw Configuration

Blk.No.	Type	Rev. or Nor.	Radius Screw	Tips	Disk Angle or Disk Thick.	Pitch or Disk No.	Turns or Disk No.	Length	Division Number Top	Flank	Axis
1.	SW	Nor..	19.5	2	0	30	4	120	2	10	20
2.	KD	Nor..	19.5	2	30	10	12	60	2	10	20
3.	KD	Rev..	19.5	2	30	10	10	50	2	10	20
4.	SW	Nor..	19.5	2	0	30	4	120	2	10	20

Input Parameters
Element Type
Self-WipingScrews
 Normal Reverse
Screw Radius(mm) 19.5
Tip number 2
Screw Pitch(mm)
Turns
Division Number
Top 2 Flank 10
Axis 20
Add

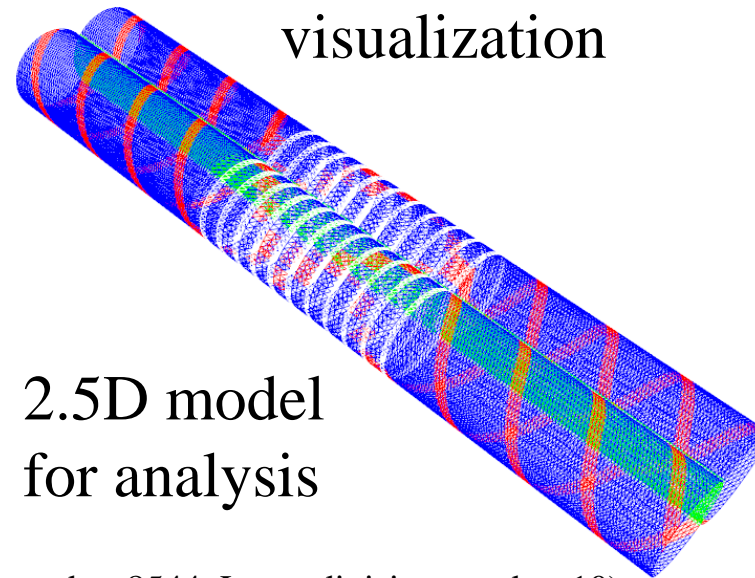
Screw Configuration Information File
test333 Save Import

Model Selection
 2.5D Analysis Model 3D Visual Model
 2D Expanded Model T->Q

Editing Button
Up Insert Delete Meshing
Down Modify All Delete Thickness Plot

View Plane
XY XZ YZ

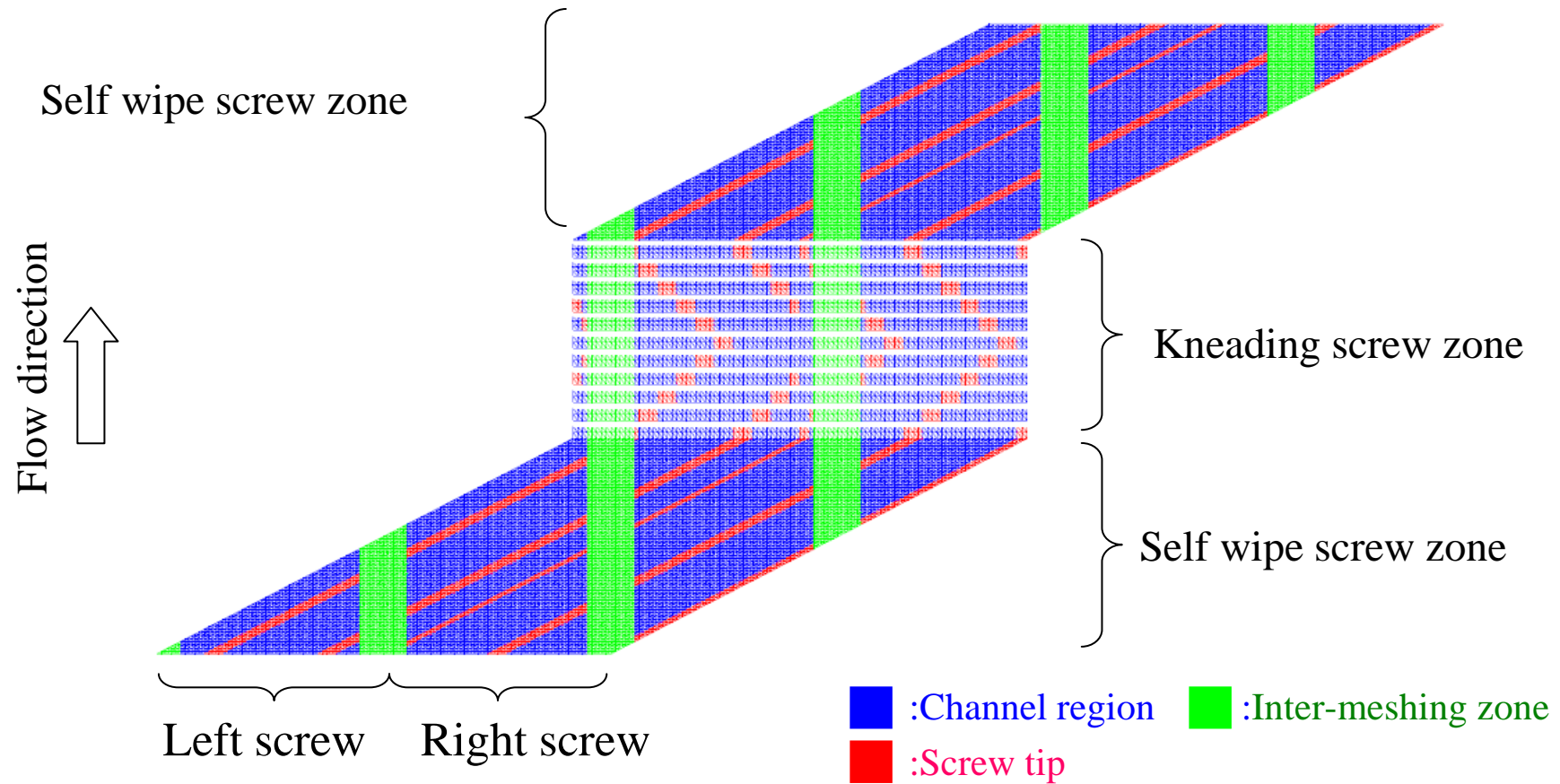
3D model for visualization



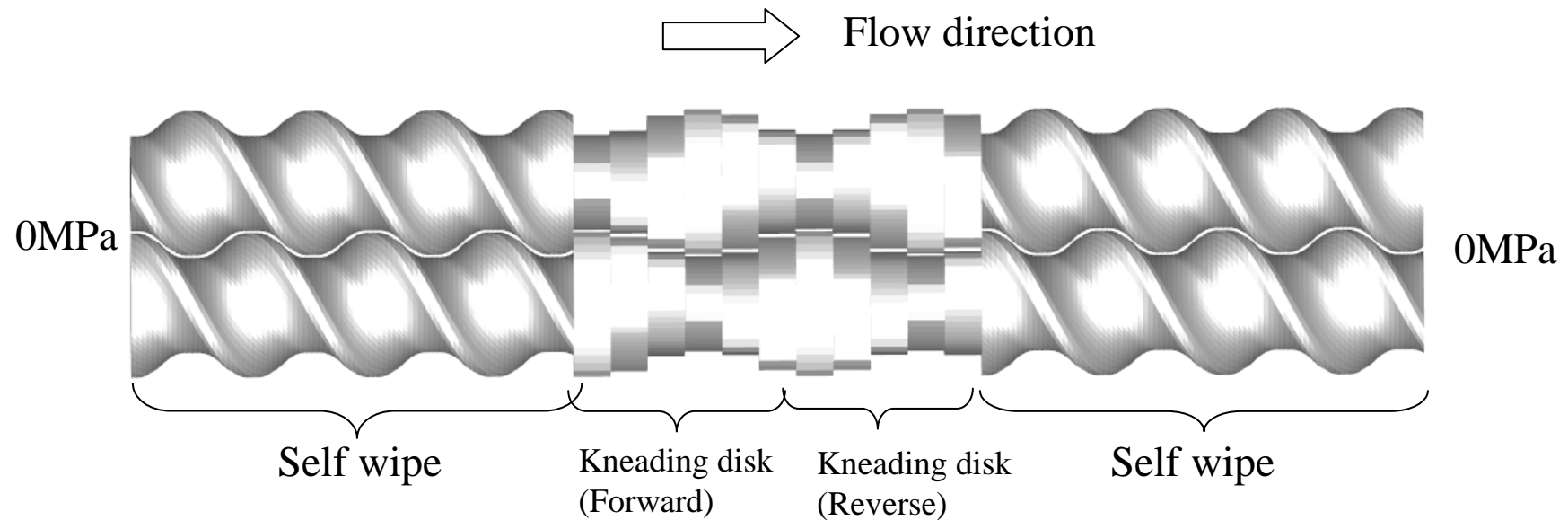
2.5D model for analysis

(Element number:16896,Node number:8544, Layer division number:10)

UV unwound FEA model



□ Test example



Intermeshing co-rotating twin screw extruder

Screw rotational	100 rpm
Material	Newtonian ($\eta = 1000 \text{Pa} \cdot \text{s}$)
Calculation cycle	48 (corresponding to the mesh division number in the circumferential direction)

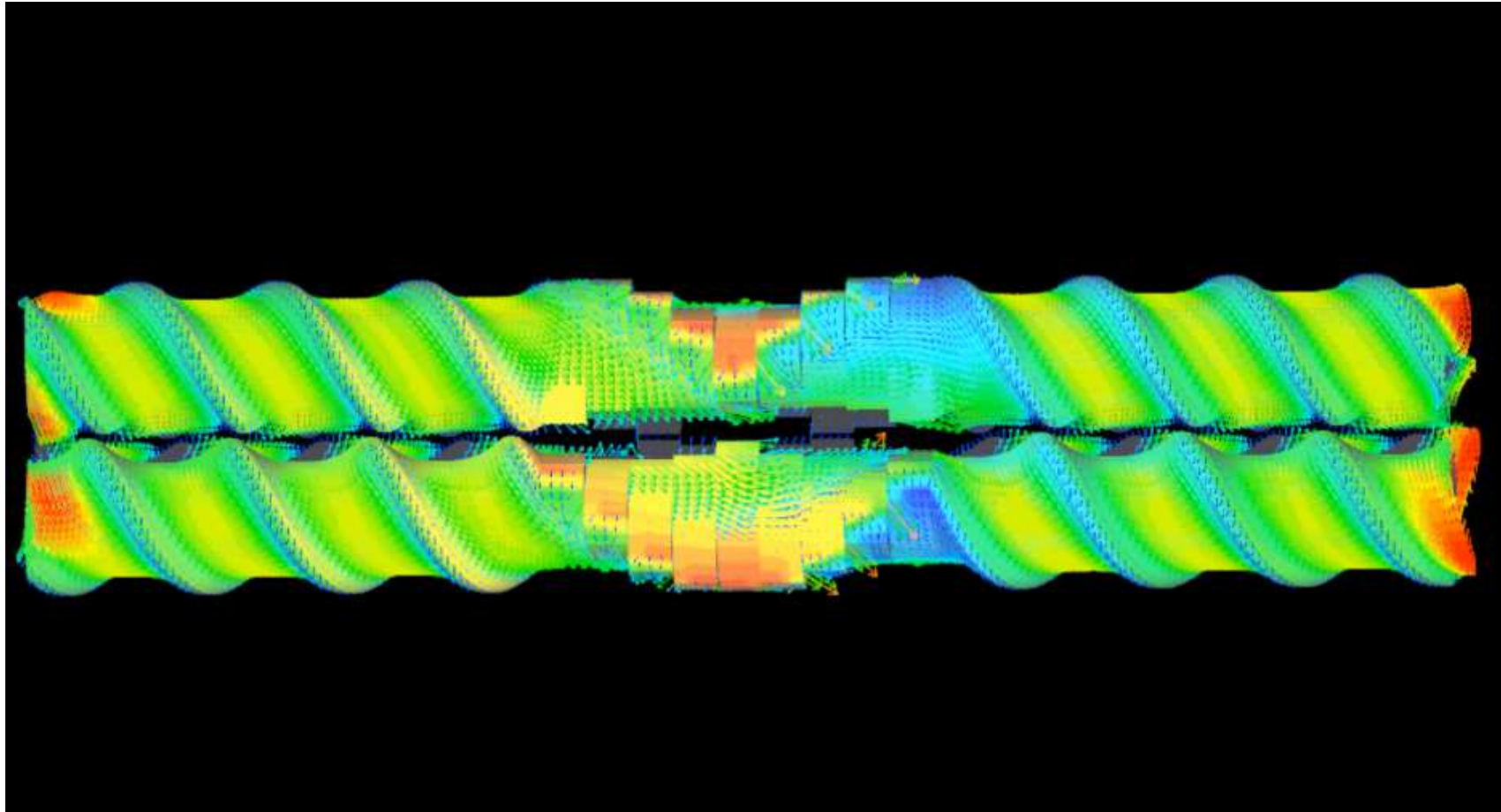
List of the time consumption for a simulation

Operation	Time consumption
Pre-processing	Ignorable(<1 minute for numeric parameter input)
Analysis	CPU time : 40 sec (for 48 cycles flow simulation)
Post-processing (Particle trace simulation to estimate the stream line in a snap shot information)	Turn around time : 10 sec (200 particles,1500 cycles calculation)
Post-processing (Particle trace simulation to estimate the particle path line in periodic flow fields)	Turn around time: 7 minutes (30 ~ 5430 particles,7500 cycles calculation:60 rotations)

(Computation environment: DELL Studio XPS 8100, 2.80GHz, 4.00GB)

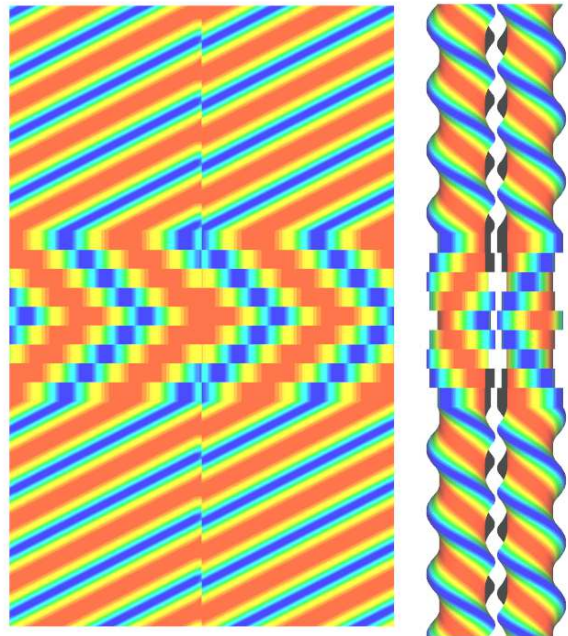


Flow direction

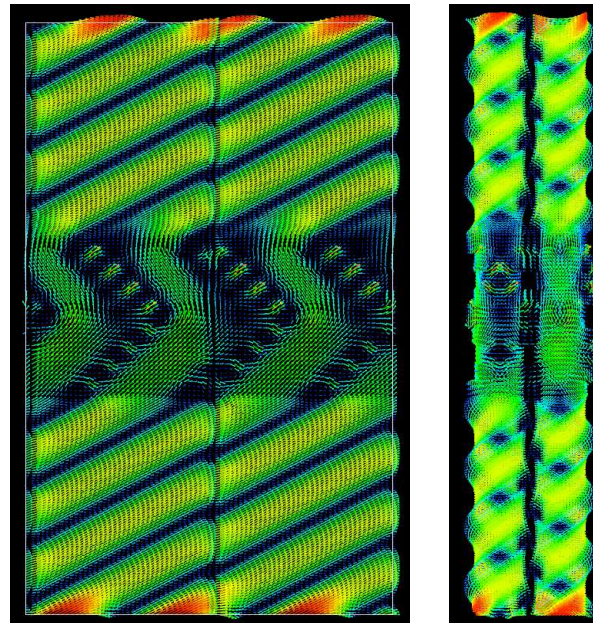


Animation 1: Pressure distribution & flow field in an intermeshing co-rotating twin screw extruder

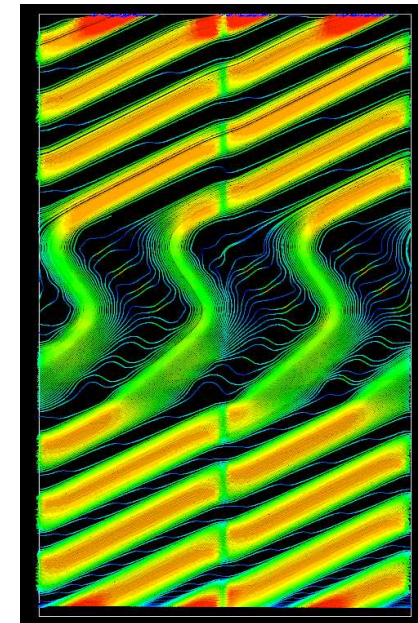
UV mapping information



UV unwound model 3D model
Channel thickness

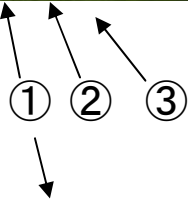
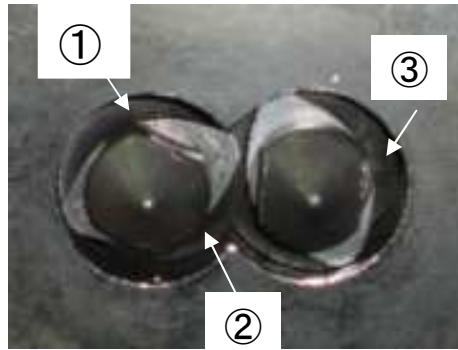


UV unwound model 3D model
Flow vector

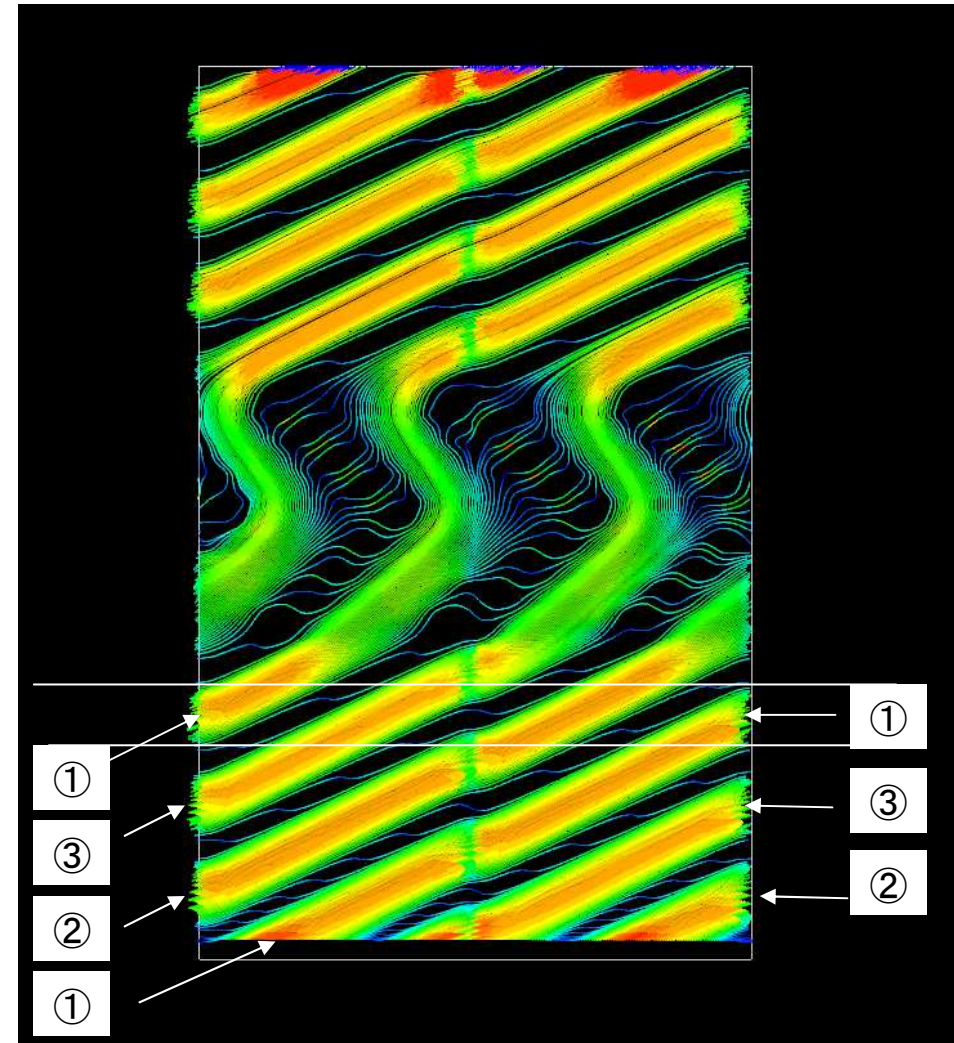


UV unwound model
Stream line in a snap
shot information

Translation of the numerical results into various models

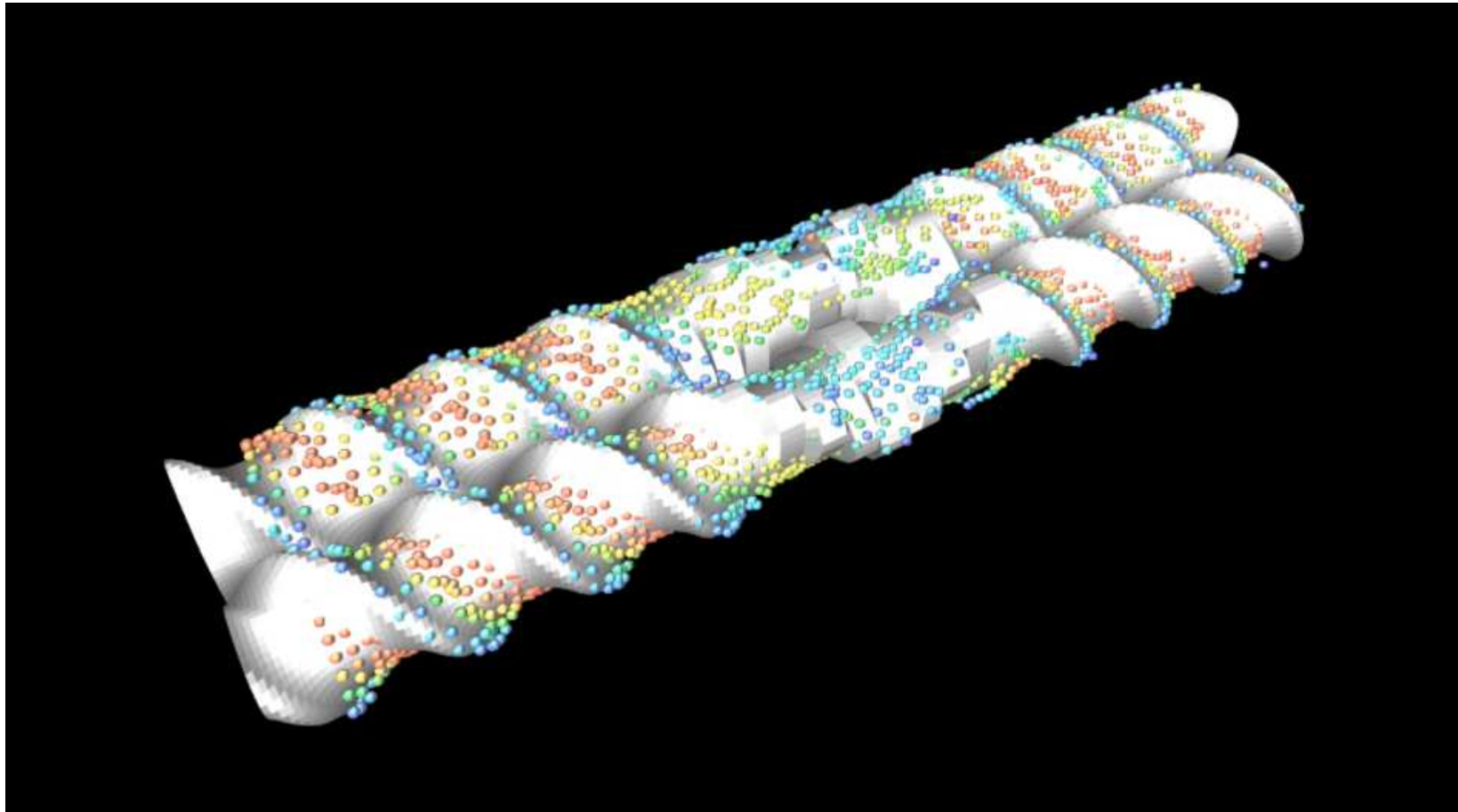


Experimental information



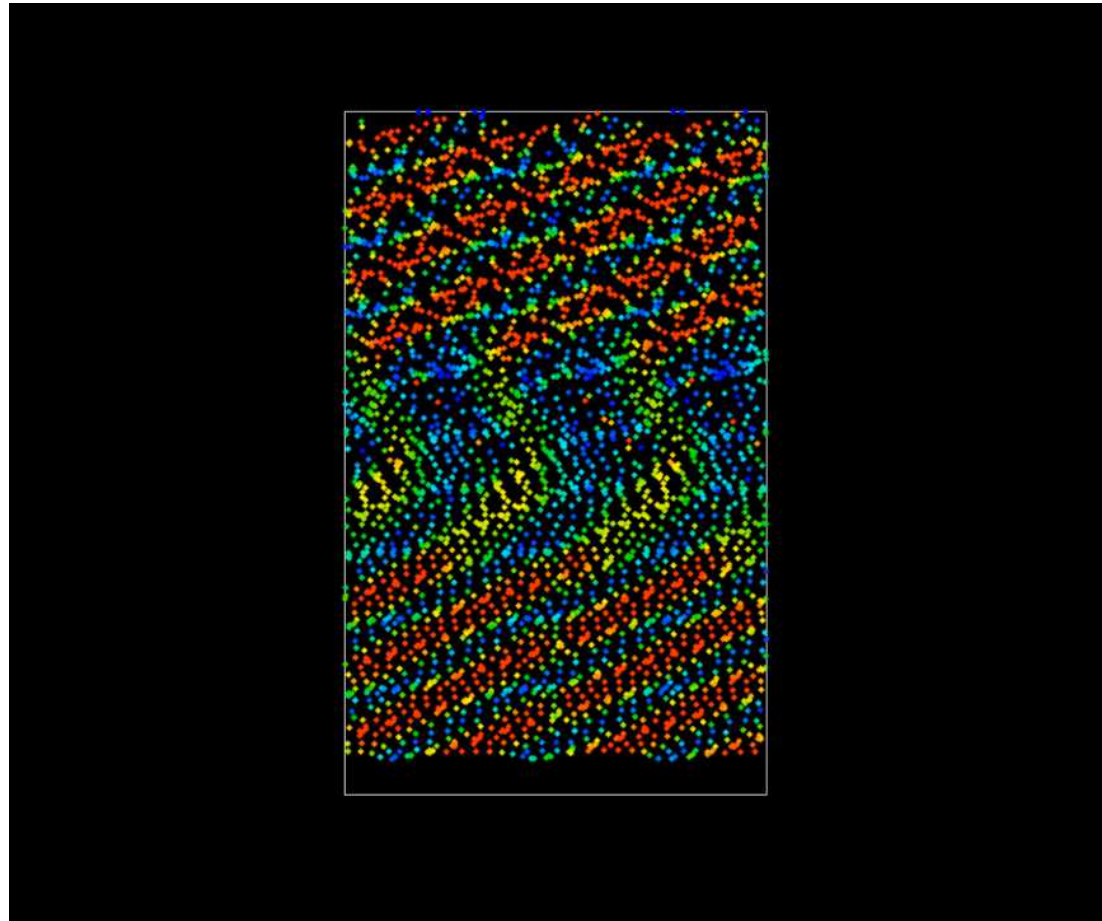
Stream line information mapped on the UV unwound model

Particle path trace simulation (3D visualized information)



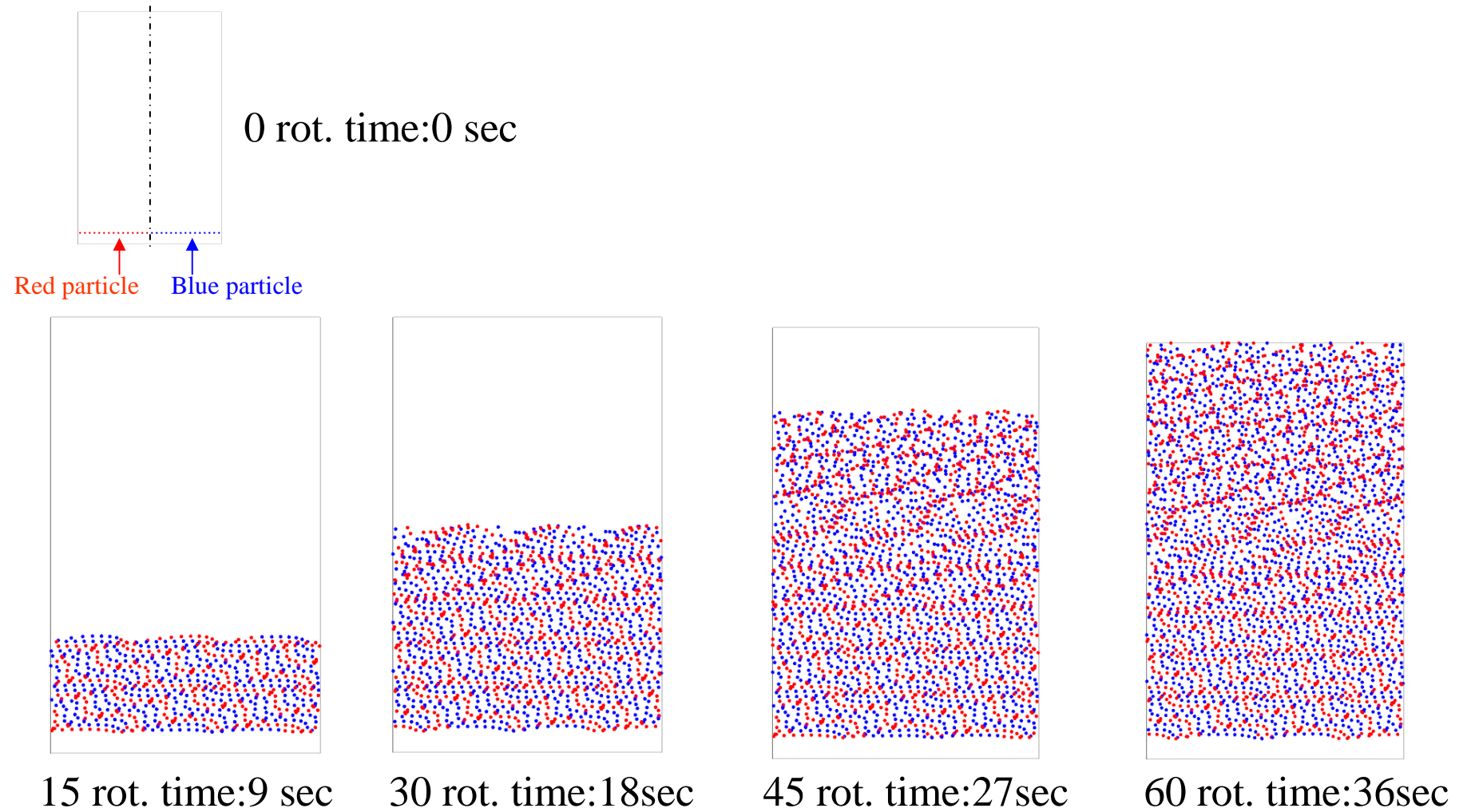
Animation 2: Result of the particle trace simulation in an intermeshing co-rotating twin screw extruder (3D visualized information)

Particle path trace simulation (UV mapping information)

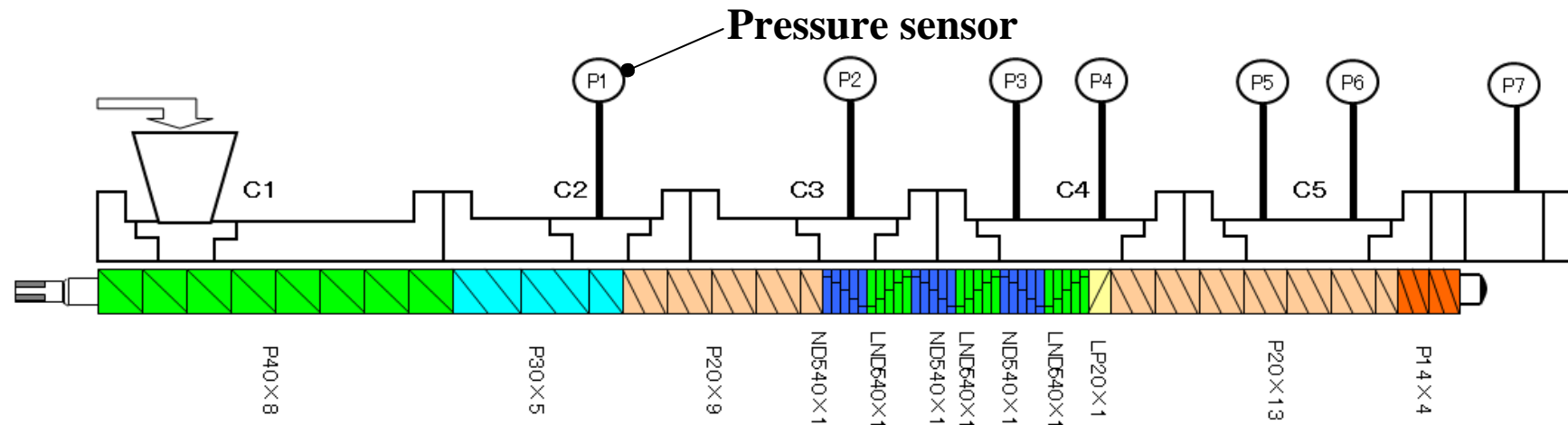


Animation 3: Result of the particle trace simulation in an intermeshing co-rotating twin screw extruder (Mapping information on the UV expanded unwound model)

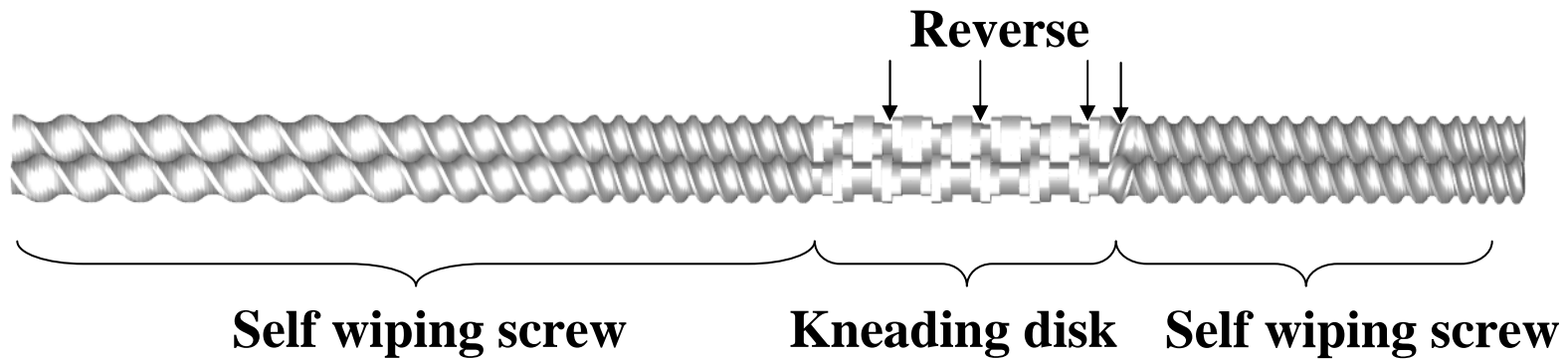
Time variation of the mixing pattern



□ Experimental verification

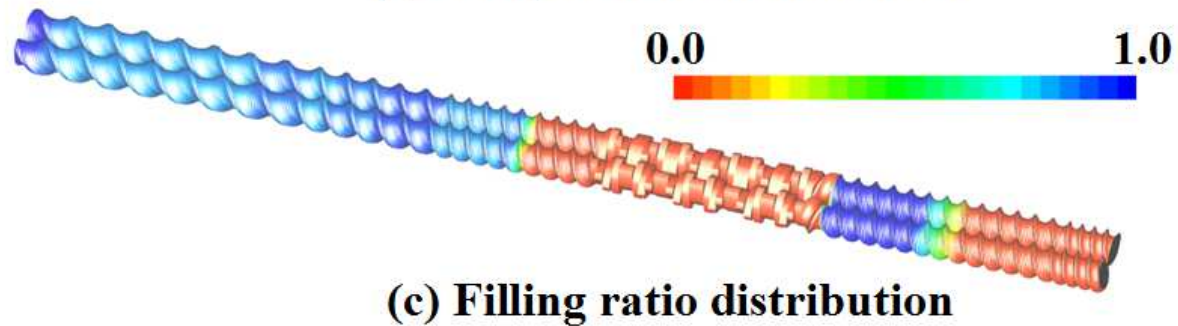
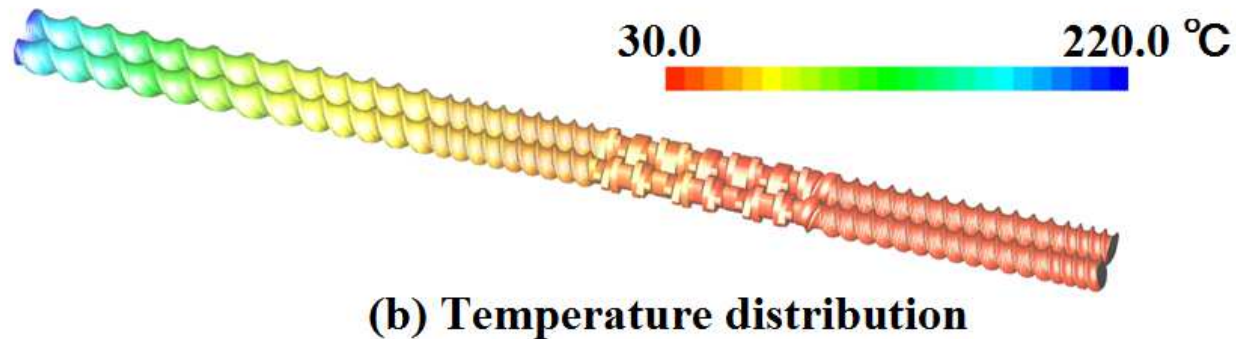
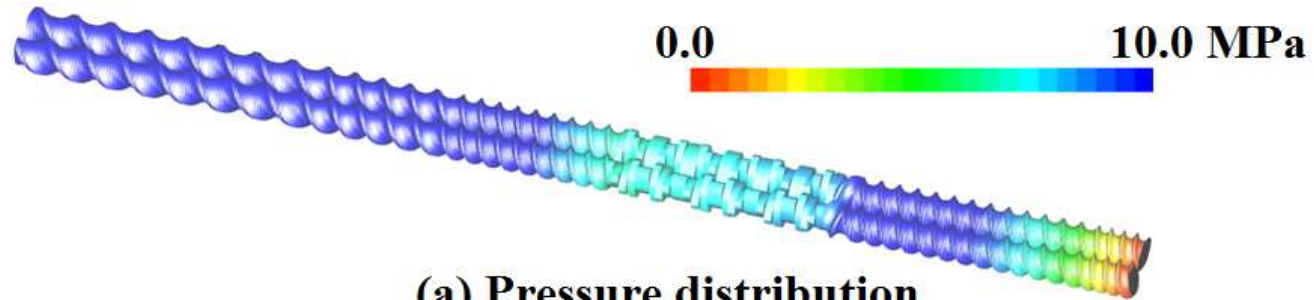


Layout of the testing machine

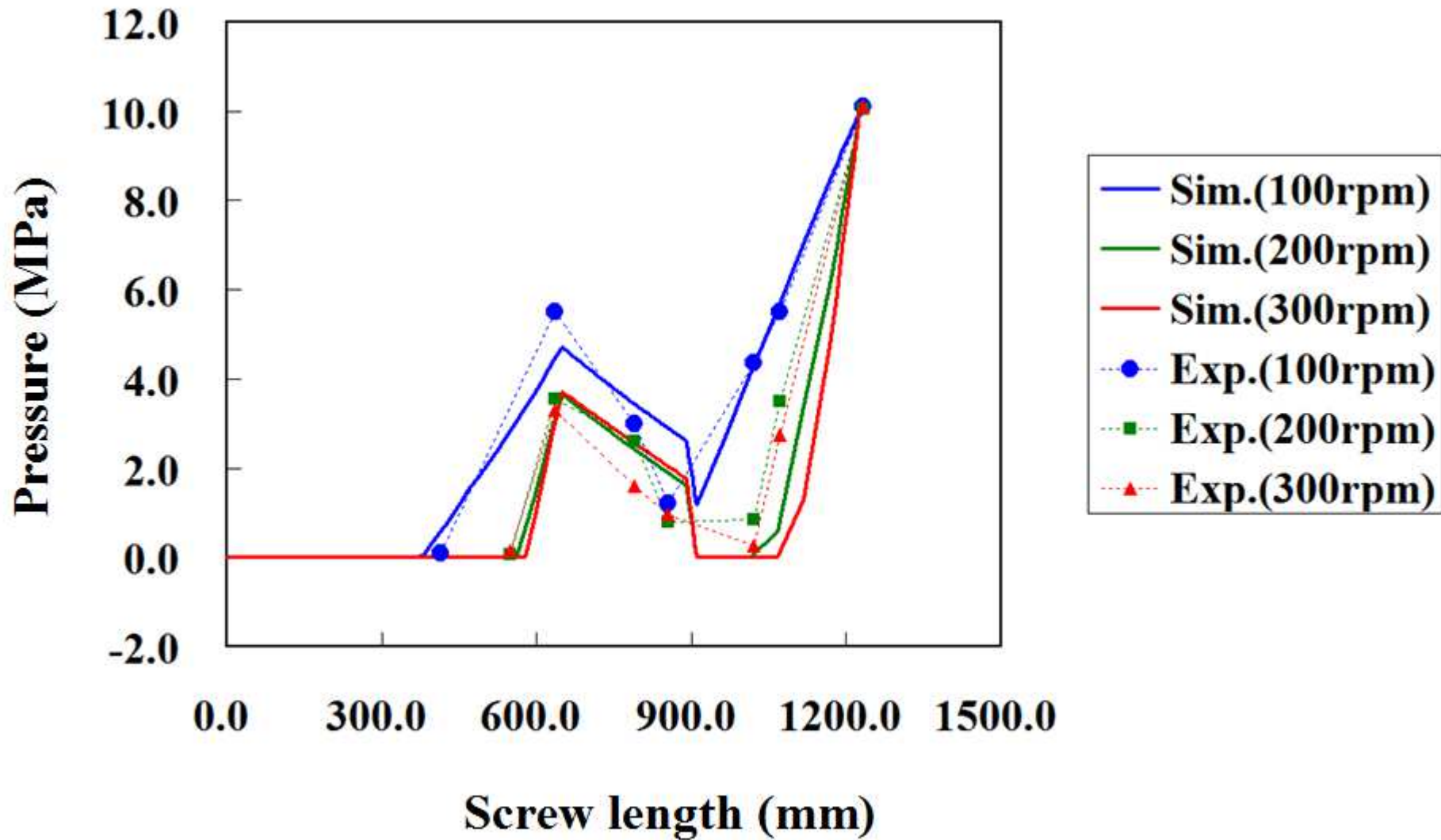


FEA model

Results of the thermal flow distribution



Experimental verification of the predicted pressure



□ Conclusions

成果：

- ・一般化Hele-Shaw流れの定式化及びメッシュ生成技術を併用することで二軸スクリュ押出機の効率的な解析法を構築した。
- ・実験検証解析を通じて解析結果の妥当性を検討した。

今後の課題：

- ・パーティルトレース機能の改良（滞留時間分布、混合効率、動的溶融可塑化モデル）
- ・検証解析の継続
- ・異方向噛合型スクリュ、コニカルタイプ等への用途展開

謝 辞

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